



**JOINT IMPLEMENTATION PROJECT DESIGN DOCUMENT FORM**  
**Version 01 - in effect as of: 15 June 2006**

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**SECTION A. General description of the project**

**A.1. Title of the project:**

Nitrous Oxide Emission Reduction Project at GP Nitric Acid Plant in AB Achema Fertiliser Factory

Version number of the document: PDD v.10

Date: 12.12.2008

**A.2. Description of the project:**

The objective of this project is to reduce N<sub>2</sub>O emissions from Achema GP (Grande Paroisse) nitric acid production plant by utilizing secondary catalyst technology that converts N<sub>2</sub>O into Oxygen (O<sub>2</sub>) and Nitrogen (N<sub>2</sub>) - zero global warming potential gases. BASF technology of catalytic destruction will be used for this purpose. Project activity will not effect other emissions such as NO<sub>x</sub> or nitric acid production.

Nitrous Oxide (N<sub>2</sub>O) is a greenhouse gas, which is formed as a by-product of the nitric acid (HNO<sub>3</sub>) production process in nitric acid production plants. In order to produce nitric acid, ammonia (NH<sub>3</sub>) is oxidized in a reactor with the precious metal (platinum-rhodium) catalyst gauzes into NO – desired product. NO then is oxidized to NO<sub>2</sub> which is absorbed in water to form HNO<sub>3</sub>. N<sub>2</sub>O, formed during the process is emitted to the atmosphere as a tail gas.

In order to calculate N<sub>2</sub>O emission reductions from the project, ABB continuous multi-component measuring system Advance Cemas-NDIR is installed and operated.

**A.3. Project participants:**

Countries/Parties involved	Legal entities, participating in the project	Please indicate, if the Party involved wishes to be considered as project participant (Yes/No)
Lithuania (Host party)	AB Achema	No

AB Achema is the largest Nitrogen fertiliser plant in Lithuania and Baltic states. Annual fertiliser production exceeds 2 million tons. The plant also produces compound fertilisers, adhesives, paints, resins, industrial gases, other chemical products and intermediates. Project is implemented in a GP Nitric acid production plant of the AB Achema fertiliser factory.

**A.4. Technical description of the project:**

**A.4.1. Location of the project:**

**A.4.1.1. Host Party(ies):**

Lithuania

**A.4.1.2. Region/State/Province etc.:**

Kaunas region

**A.4.1.3. City/Town/Community etc.:**

Rukla county, Jonalaukis village

**A.4.1.4. Detail of physical location, including information allowing the unique identification of the project (maximum one page):**

The project will be implemented in the territory of the AB Achema fertiliser factory, which is located in the central part of Lithuania near the Jonava town. The closest city Kaunas is situated about 30km southwest from Jonava. Geographic coordinates of the factory site centre are: x=6105343 y=521432.

**Figure 1 Geographical location of AB Achema fertiliser plant**

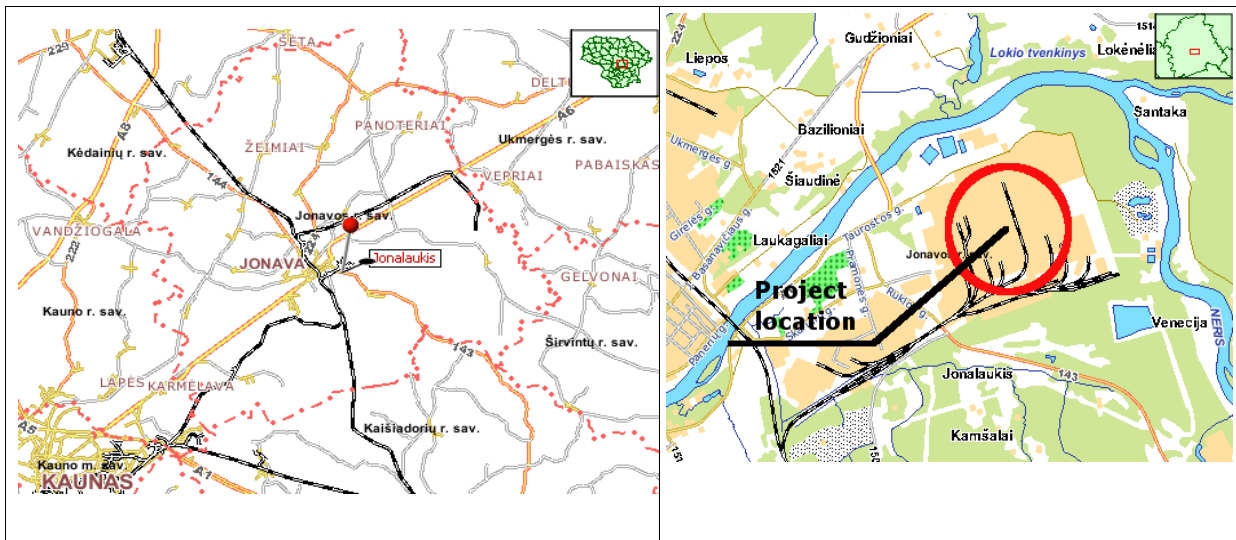


Figure 2 Physical location of AB Achema fertiliser plant

The project will be implemented in the GP Nitric acid plant within AB Achema fertiliser plant.

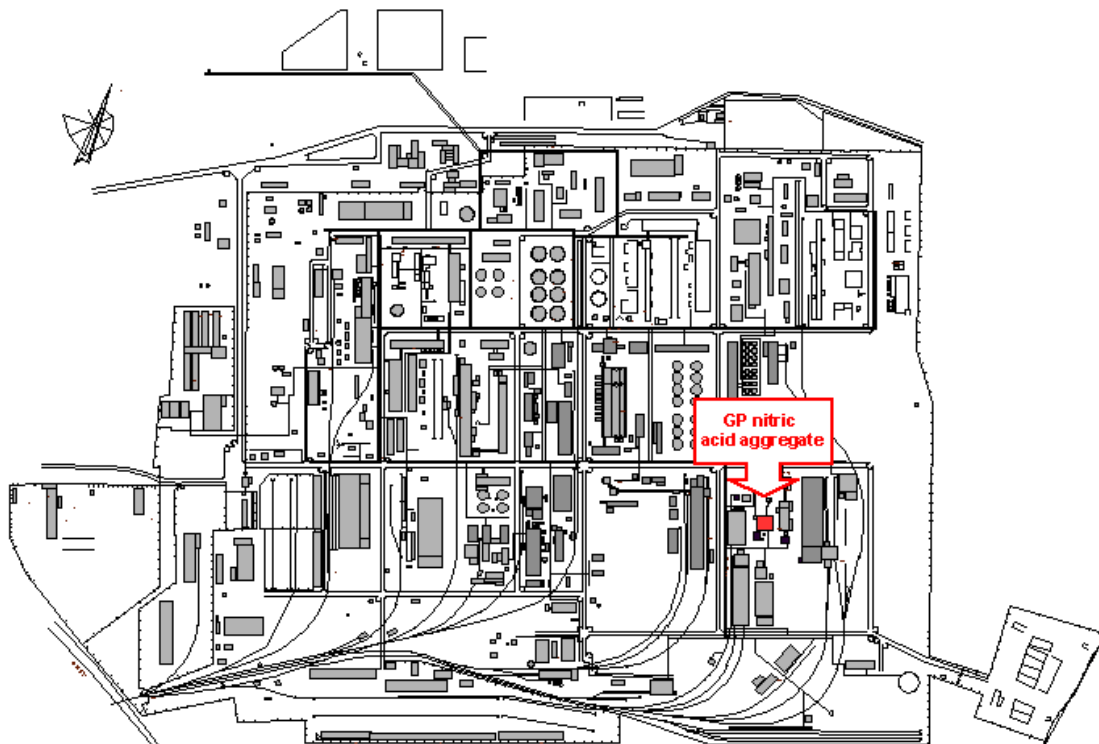


Figure 3 Location of the GP nitric acid plant within the fertiliser factory



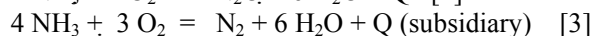
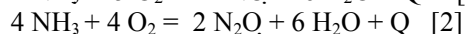
**A.4.2. Technology(ies) to be employed, or measures, operations or actions to be implemented by the project:**

*HNO<sub>3</sub> production process in GP plant*

Nitric acid is produced by burning of ammonia in four oxidation reactors. Liquid ammonia is delivered to the plant and evaporated by warming it with water in vaporizer. Then gaseous ammonia is heated in heater to the temperature of 100°C at 350 kPa pressure. Major part of ammonia of this quality is mixed with air and the other part is directed to the selective cleaning reactor.

Gaseous ammonia is delivered to the lower part of the mixer and is mixed with filtrated air that is delivered to the upper part of the mixer. Ammonia-air mixture of 160°C temperature containing 10.5% ammonia is directed to the burner.

Catalytic combustion takes place on the platinum (with palladium supplement) alloy gauzes inside the burner at 850°C temperature.



Acquired mixture of nitric oxides, water steam, nitrogen and oxygen is called nitrous gases. These gases are directed to the nitrous gas boiler for production of steam of 2 MPa pressure and 400°C temperature. Nitric oxide is further oxidized in the gas tract.



By passing heat exchangers nitrous gases cool to 180°C. Later, gases are directed and further condensed in the coolers condensers to 60°C. When temperature decreases, water steam condenses and reacts with nitric oxide in nitrous gases which leads to formation of 40-50 % nitric acid which is directed to the absorption column. Remaining nitrous gases are directed to the bottom of absorption column while demineralised water is supplied to the top of the column. Concentration of the nitric acid gradually increases while it flows down in the absorption column.



From the bottom plate acid flows to the cube of the column and further to the inflation column where remaining nitric oxides are blown from the acid and returned to the column. After crossing whole absorption column nitric gases lose nitric oxides and become tail gases of 30°C temperature and containing 0.11-0.15% nitric oxides. Tail gases are further directed to the cleaning of remaining nitric oxides.

**Table 1 Main parameters of nitric acid production at GP plant**

Process	Value
Production of HNO <sub>3</sub>	41,67 t HNO <sub>3</sub> 100% / h
Air intake to NH <sub>3</sub> burner	135.800 Nm <sup>3</sup> /h
Ammonia intake	15.500 Nm <sup>3</sup> /h
O <sub>2</sub> in tail gas	2,8 %-3,5%
N <sub>2</sub> O in tail gas	~ 1,300 – 1,400 ppm
Tail gas flow	110,000 – 150,000 Nm <sup>3</sup> /h

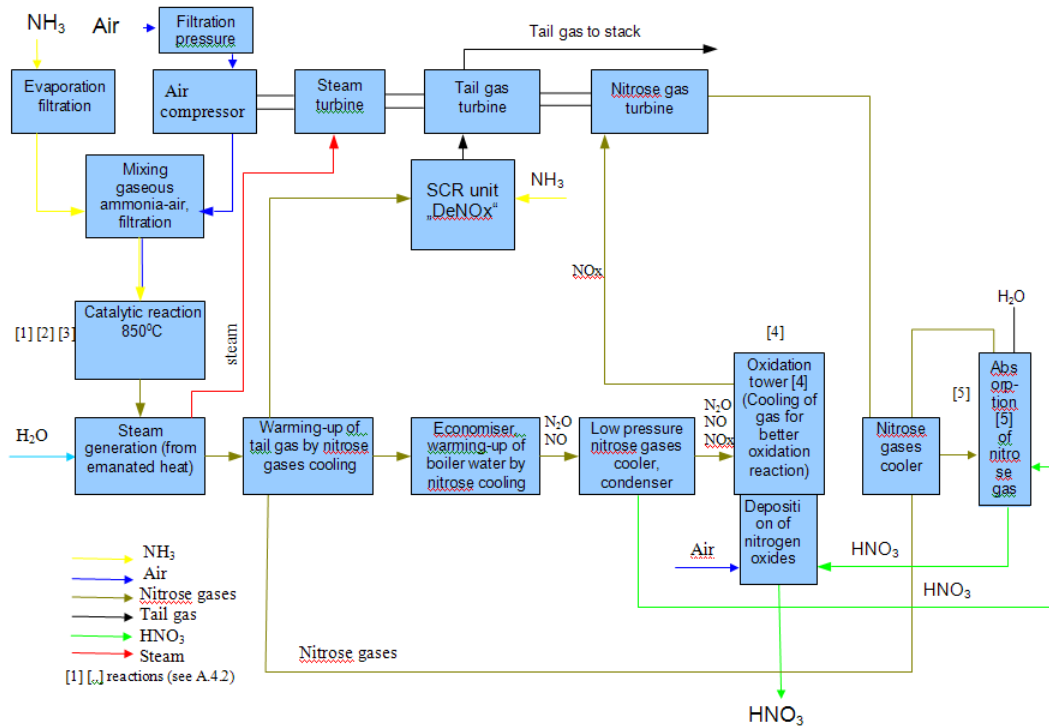


Figure 4 Nitric acid production process at GP plant

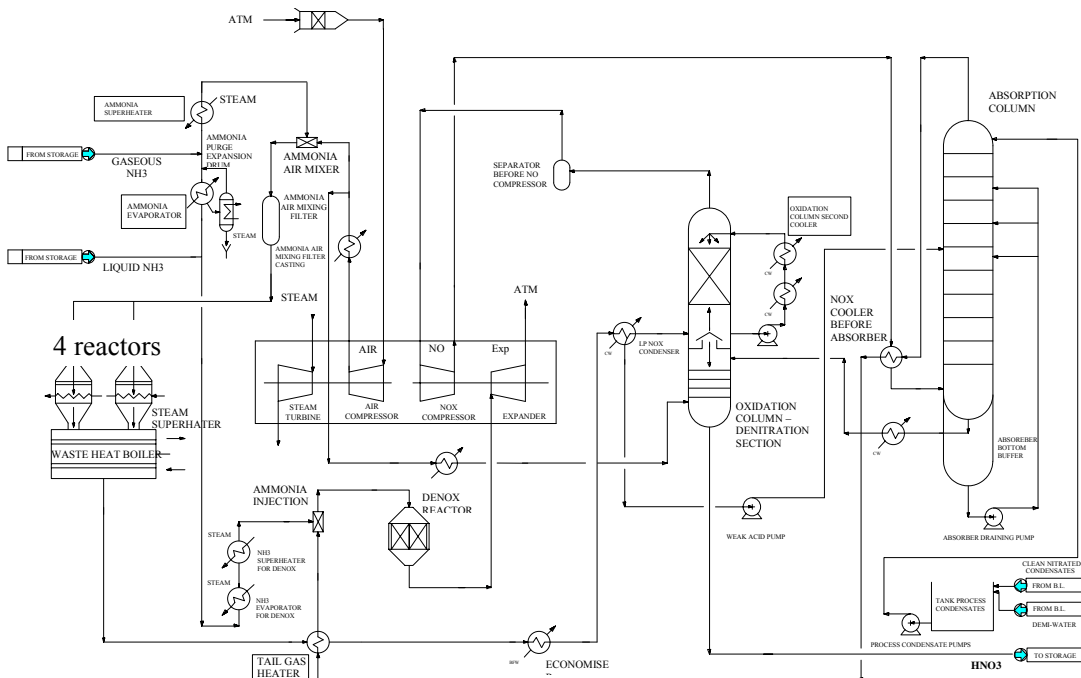


Figure 5 Nitric acid production scheme at GP plant

HNO<sub>3</sub> production process in Achema is performed in production cycles or so called campaigns. A campaign is a total time of primary catalyst (Platinum-Palladium gauzes) operation. When the primary



catalyst is worn, the installation is stopped for maintenance and the catalyst is replaced with a new one. The length of a campaign in the GP plant is about 11 months.

#### *Available N<sub>2</sub>O abatement technologies*

In the nitric acid manufacturing process N<sub>2</sub>O is inevitably generated as a by-product. The process typically generates N<sub>2</sub>O quantities at levels of 2-19 kg per tonne of 100% nitric acid. The classification of potential N<sub>2</sub>O abatement technologies at Nitric acid plants is based on the process location of the treatment device. There are three main technologies to reduce N<sub>2</sub>O emissions from HNO<sub>3</sub> production process:

*Primary* - N<sub>2</sub>O is prevented from forming in the oxidation gauzes. This requires modifications to the precious metal ammonia oxidation gauzes or utilization of another ammonia oxidization catalyst to reduce N<sub>2</sub>O formation.

*Secondary* - N<sub>2</sub>O is removed anywhere between the outlet or the ammonia oxidation gauzes and the inlet of the absorption tower. Technologies that belong to this group are:

- High Temperature Catalytic Destruction in oxidation reactor (>800° C)
- Homogeneous decomposition in reactor

*Tertiary* - N<sub>2</sub>O is removed at the tail gas, after the absorption tower and previous to the expansion turbine. Technologies that use tertiary process are:

- Low Temperature Catalytic Destruction in tail gas (<400° C)
- Non-selective catalytic reduction in tail gas
- Thermal destruction in tail gas

#### *N<sub>2</sub>O abatement technology applied in the GP plant*

After thorough evaluation of potential technologies for the reduction of N<sub>2</sub>O emissions at Achema plant, a secondary catalyst technology of catalytic destruction in the reactor has been selected. The project activity comprises the installation of secondary catalysts in the oxidation reactors of the nitric acid plant GP at Achema. Some advantages specific to the selected secondary catalyst are:

- No significant effect on nitric oxide yield.
- Level of N<sub>2</sub>O in tail gas is achievable by adjusting the catalyst bed thickness.
- Considerable performance compared to other technologies

BASF technology will be applied by introducing a new catalyst bed which is installed in a new basket, directly under the Platinum gauze in the nitric acid reactors. The technology is owned and patented by BASF (German patent BASF Catalysts 03-80, 03-85 and 03-86), and has also been installed in several other plants.

The secondary catalyst (on Al<sub>2</sub>O<sub>3</sub> basis with active metal oxides CuO and ZnO) will be installed underneath the platinum gauze. 20-100 mm additional free space under the Platinum gauze is required. For this purpose a reconstruction of burner basket is needed to make required space. The reconstruction and installation will be done during the planned shut down for maintenance of the GP plant. The lifetime of the secondary catalyst is about 3 campaigns (lifetime of the platinum gauze), i.e. - about 550 days in the high-pressure nitric acid reactors and about 1000 days in the medium-pressure nitric acid reactors. The expected efficiency of the secondary catalyst is up to 80%.

**A.4.3. Brief explanation of how the anthropogenic emissions of greenhouse gases by sources are to be reduced by the proposed JI project, including why the emission reductions would not occur in the absence of the proposed project, taking into account national and/or sectoral policies and circumstances:**

N<sub>2</sub>O emissions at Achema fertiliser plant will be reduced by installing BASF secondary catalyst in 4 oxidation reactors of GP nitric acid production plant. The catalyst is expected to work with up to 80% efficiency - hence the baseline emissions will be reduced by the corresponding amount.

The Baseline scenario is considered to be a continuation of nitric acid production in GP plant in business as usual case i.e. with the current technologies and levels of N<sub>2</sub>O emissions. N<sub>2</sub>O limit values are not set in the IPPC permit issued to AB Achema so the company currently is not obliged to consider abatement of N<sub>2</sub>O emissions in any way. Capture of N<sub>2</sub>O as a potential product is not feasible because N<sub>2</sub>O flow contains impurities and has variable concentrations that would imply complex purification and concentration units in order to produce potentially marketable N<sub>2</sub>O. The feasibility of using the nitric acid tail gas containing N<sub>2</sub>O as a feedstock for the petrochemical industry has not been demonstrated. Thus, from the economic perspective, installation of secondary catalyst in the nitric acid production plant is a costly task that gives revenues only within the framework of Kyoto flexible mechanisms i.e. does not give any other benefits apart from revenues related to ERU sales.

The baseline can be influenced by legal or other developments that might occur on a later stage of the project development. For example a new regulation can come into effect imposing requirements for N<sub>2</sub>O reduction, or N<sub>2</sub>O limit values can be set in Achema's IPPC permit. Any of such developments will be reflected and the baseline will be adjusted according to the new requirements (i.e. if limit values are set in the IPPC permit, these values will be set as a new baseline).

Baseline emissions are monitored and calculated by continuous multi-component measuring system Advance Cemas-NDIR manufactured by ABB, and installed prior to secondary catalysts. The monitoring system will allow to measure N<sub>2</sub>O concentration in the tail gas flow continuously during the entire lifespan of the primary catalysts in the oxidation reactor i.e. for 11 months, starting June 2007<sup>1</sup>. Monitoring results will give an average value of N<sub>2</sub>O emissions released to the atmosphere while producing 1 ton of HNO<sub>3</sub> without abatement technique. After the installation of the secondary catalyst, the baseline emissions will be compared to the actual emissions that will be continuously measured. The difference between baseline emissions and actually measured emissions will give emission reduction values.

**A.4.3.1. Estimated amount of emission reductions over the crediting period:**

**Table 2 Estimated emission reductions**

	Years
<b>Crediting period</b>	<b>4 years and 4,5 months (16.08.2008 – 31.12.2012)</b>
<b>Year</b>	<b>Estimate of annual emission reductions in tonnes of CO<sub>2</sub> equivalent</b>

<sup>1</sup> The monitoring of the baseline combines two campaigns as described in section B1





2008	241,964
2009	578,569
2010	578,569
2011	578,569
2012	487,913
Total estimated emission reductions over the crediting period (tonnes of CO <sub>2</sub> equivalent)	2,465,585
Annual average of estimated emission reductions over the crediting period (tonnes of CO <sub>2</sub> equivalent)	563,562

#### **A.5. Project approval by the Parties involved:**

Letter of Endorsement (LoE) was issued to Achema's N<sub>2</sub>O reduction JI project by the Ministry of Environment on 8<sup>th</sup> January 2007, by communication No. (10-5)-D8-216. The evaluation of the Project Idea Note was made in consideration of provisions settled out in the regulation for JI project implementation in Lithuania (JI regulation), approved by the ordinance No D1-183 of the Minister of Environment of the Republic of Lithuania on 1<sup>th</sup> April 2006 (Official Gazette, 2005 No 50-1671). Also the assent from the Lithuanian Environmental Investment Fund was taken into consideration in the decision making procedure. The ordinance no D1-183 of the Minister of Environment of the Republic of Lithuania on 1<sup>th</sup> April 2006, appoints Lithuanian Environmental Investment Fund to perform activities of the National Agency.

According to the JI regulation:

10. In order to make the decision specified in Par. 9, the Ministry of Environment shall submit the concept to the National Agency for evaluation.

11. The National Agency shall take into account the criteria for the joint implementation of feasible priority projects listed in the Strategic Tracks, the preferences of the national strategic documents and conditions listed in the Regulations; further it shall evaluate the concept and, within 45 (forty-five) days, provide the Ministry of Environment with the conclusion concerning acceptability of the concept of the provided Project and its further development.

### **SECTION B. Baseline**

#### **B.1. Description and justification of the baseline chosen:**

In order to set the baseline for the Achema GP JI project, the approved baseline methodology AM0034 "Catalytic reduction of N<sub>2</sub>O inside the ammonia burner of nitric acid plants" shall be applied. The methodology can be found on the UNFCCC website at the following link:  
<http://cdm.unfccc.int/methodologies/PAmethodologies/approved.html>

The AM 0034 methodology is applicable to Achema GP JI project, because the project complies with all applicability requirements set in the methodology:



- ✓ Existing nitric acid production facilities at Achema fertiliser plant were installed earlier than 31 December 2005
- ✓ The project activity will not result in the shut down of any existing N<sub>2</sub>O destruction or abatement facility or equipment in the plant
- ✓ The project activity shall not affect the level of nitric acid production (the manufacturer of secondary catalyst technology – BASF, guarantees that the level of nitric acid production will not be affected)
- ✓ There are currently no regulatory requirements or incentives to reduce levels of N<sub>2</sub>O emissions from nitric acid plants in Lithuania (N<sub>2</sub>O is not regulated by IPPC permits or any other legislation).
- ✓ No N<sub>2</sub>O abatement technology is currently installed in the plant
- ✓ The project activity will not increase NO<sub>x</sub> emissions (assured by the manufacturer)
- ✓ NO<sub>x</sub> abatement catalyst installed, if any, prior to the start of the project activity is not a Non-Selective Catalytic Reduction (NSCR) DeNO<sub>x</sub> unit (assured by the manufacturer)
- ✓ Operation of the secondary N<sub>2</sub>O abatement catalyst installed under the project activity does not lead to any process emissions of greenhouse gases, directly or indirectly (assured by the manufacturer).
- ✓ Continuous real-time measurements of N<sub>2</sub>O concentration and total gas volume flow can be carried out in the stack:
  - Prior to the installation of the secondary catalyst for one campaign, and
  - After the installation of the secondary catalyst throughout the chosen crediting period of the project activity

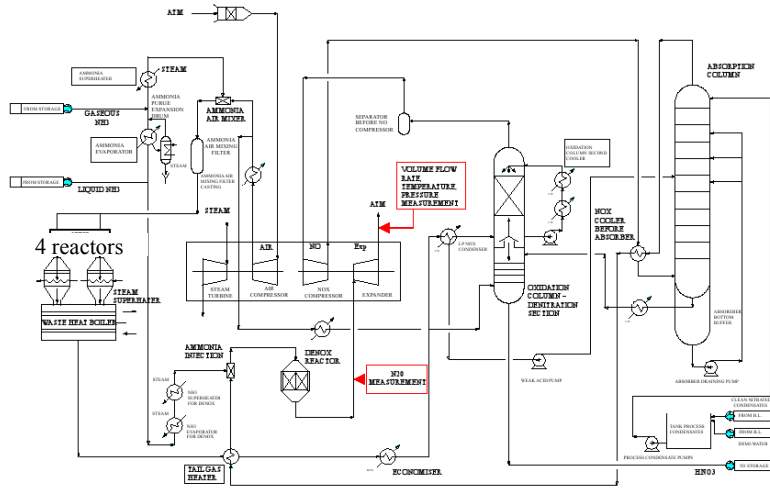
The N<sub>2</sub>O monitoring system is designed according to the requirements set in the approved CDM baseline methodology AM0034 .

Baseline emissions will be monitored and calculated by installing continuous multi-component measuring system Advance Cemas-NDIR manufactured by ABB, prior to installation of secondary catalysts. The monitoring system will allow to measure N<sub>2</sub>O concentration in the tail gas flow continuously during the entire lifespan of the primary catalysts in the oxidation reactor i.e. for 11 months.

The monitoring system was installed, adjusted and launched on 30<sup>th</sup> June 2007 at the end of campaign IV (campaign IV ended on 19<sup>th</sup> August 2007). Campaign V (baseline campaign) was launched on 5<sup>th</sup> September 2007. Emissions will be monitored during the entire baseline campaign after which, a secondary catalyst will be installed and the first project campaign (VI) will be launched.

Monitoring results of the baseline campaign will give an average value of N<sub>2</sub>O emissions released to the atmosphere while producing 1 ton of HNO<sub>3</sub> without abatement technique. After the installation of the secondary catalyst, the baseline emissions will be compared to the actual emissions that will be continuously measured. The difference between baseline emissions and actual emissions after the installation of the secondary catalyst will give emission reduction values.

Location of sampling probes for on-line measurement of tail gas volume flow, temperature, pressure and N<sub>2</sub>O concentration with ABB multi-component measuring system at GP nitric acid plant are shown in a figure below.



**Figure 6 Sampling points for N<sub>2</sub>O monitoring at GP plant**

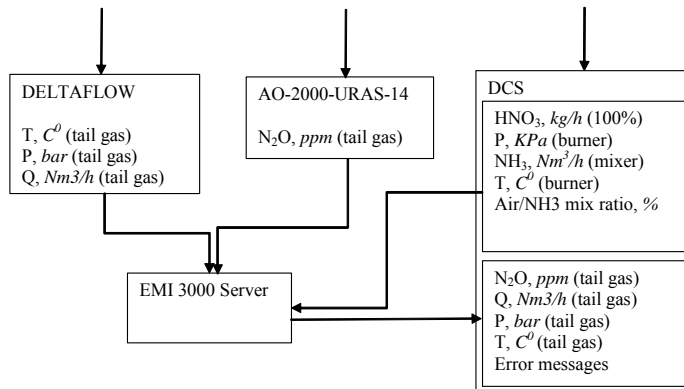
As it can be seen on the process scheme above, the volume flow, temperature and pressure measuring probe will be installed after expander unit and N<sub>2</sub>O sampling probe directly after DeNO<sub>x</sub> reactor.

Part of the volume flow rate monitoring system is also the measurement of the gas temperature and gas pressure. Technical details of monitoring equipment for N<sub>2</sub>O concentration measurement are described below. Flow volume, temperature and pressure of the tail gas are measured separately from N<sub>2</sub>O because length of straight duct at the N<sub>2</sub>O sampling point is not long enough according to requirements for such measurements.

The N<sub>2</sub>O monitoring system at GP plant is comprised of:

- ✓ N<sub>2</sub>O analyzer AO-2000-URAS-14 (ABB)
- ✓ Flow meter DELTAFLOW (Systec)
- ✓ Data Server EMI 3000
- ✓ Distributed control system (DCS)

A simplified scheme of the monitoring system is presented below:



**Figure 7 Automated monitoring system at GP plant**

A flow meter measures volume flow (m<sup>3</sup>/h), temperature and pressure in the tail gas and sends signals to the server. The server stores data and forwards signal to the Distributed Control System (DCS). The N<sub>2</sub>O



analyzer continuously measures concentration of N<sub>2</sub>O in the tail gas and also sends signal to the data server which forwards it to DCS.

The AM0034 methodology requires monitoring scheme to be installed according to the European Norm 14181 (2004). The Norm requires evaluation of the automated measuring system (AMS) against three Quality Assurance Levels (QAL1, QAL2 and QAL3) and an Annual Surveillance Test (AST). Besides that, it must be ensured that the automated measuring system (AMS) is installed in accordance with the relevant European/ international standards and manufacturer requirements and functional test is performed at the commissioning of the AMS.

QAL1 procedure requires compliance of the equipment with EN ISO 14956. AO-2000-URAS-14 and DELTAFLOW are ISO 14956 certified by the manufacturers.

QAL2 procedure requires determination of the calibration function and a test of the measured values of the AMS compared with the uncertainty given by legislation. During the maintenance period of the GP plant (September 2007) the openings required for QAL2 tests will be made in the duct. QAL2 procedure will be performed by an accredited independent entity at the end of the next campaign.

QAL3 is a procedure to check drift and precision in order to demonstrate that the AMS is in control during its operation so that it continues to function within the required specifications for uncertainty. QAL3 procedures will be performed automatically as the system will calibrate itself once a week. In addition, Achema experts will perform maintenance of the equipment – will fix faults, change filters, remove condensate from the system etc.

AST is a procedure to evaluate whether the measured values obtained from the AMS still meet the required uncertainty criteria – as demonstrated in the previous QAL2 test. AST will be performed annually by the selected validator.

The AM0034 requires to determine the normal ranges for operating conditions for the following parameters: (i) oxidation temperature; (ii) oxidation pressure; (iii) ammonia gas flow rate, and (iv) air input flow rates. To calculate the “permitted range” for oxidation temperature and pressure, a historical data method was chosen. It should be noted that neither legislation in Lithuania nor the internal regulation of AB Achema requires keeping records of the concerned data longer than for 1 year. Therefore, historical data in concern is available from 01.04.2005 in records for every 12 hours.

According to the AM0034 methodology, the permitted range of operating temperature and pressure is assigned as the historical minimum (value of parameter below which 2.5% of the observation lie) and maximum operating conditions (value of parameter exceeded by 2.5% of observations). The calculations, gave the following results:

**Table 3 Permitted data range based on historical data**

	Oxidation temperature (°C )				Oxidation pressure (Mpa)	NH <sub>3</sub> flow rate (m <sup>3</sup> NH <sub>3</sub> /H)	Air-NH <sub>3</sub> ratio (%)
	D101/A	D101/B	D101/C	D101/D			
Historical maximum	769.5	778.0	778.7	777.2	0.283	15149.2	10.1
Historical minimum	756.0	764.1	765.2	761.4	0.243	12679.4	9.3

After the baseline monitoring period is over, records of the monitored data (N<sub>2</sub>O concentration and tail gas flow volume) shall be statistically examined according to AM0034 methodology:



- a) Sample mean ( $\bar{x}$ ) calculated
- b) Sample standard deviation ( $s$ ) calculated
- c) 95% confidence interval (equal to 1.96 times the standard deviation) calculated
- d) All data that lie outside the 95% confidence interval will be eliminated
- e) New sample mean from the remaining values (volume of stack gas (VSG) and  $N_2O$  concentration of stack gas (NCSG)) will be calculated

The average mass of  $N_2O$  emissions per hour will be estimated as product of the NCSG and VSG. The  $N_2O$  emissions per campaign will be estimated as product of  $N_2O$  emission per hour and the total number of complete hours of operation of the campaign using the following equation:

$$BE_{BC} = VSG_{BC} * NCSG_{BC} * 10^{-9} * OH_{BC} \quad (tN_2O) \quad (1)$$

The plant specific baseline emissions factor representing the average  $N_2O$  emissions per tonne of nitric acid over one full campaign will be derived by dividing the total mass of  $N_2O$  emissions by the total output of 100% concentrated nitric acid for that period. The overall uncertainty of the monitoring system shall also be determined and the measurement error will be expressed as a percentage (UNC). The  $N_2O$  emission factor per tonne of nitric acid produced in the baseline period (EF<sub>BL</sub>) shall then be reduced by the estimated percentage error as follows:

$$EF_{BL} = (BE_{BC} / NAP_{BC}) (1 - UNC/100) \quad (tN_2O/tHNO_3) \quad (2)$$

where:

EF<sub>BL</sub> - Baseline  $N_2O$  emissions factor (t $N_2O$ /t $HNO_3$ )

BE<sub>BC</sub> - Total  $N_2O$  emissions during the baseline campaign (t $N_2O$ )

NCSG<sub>BC</sub> - Mean concentration of  $N_2O$  in the stack gas during the baseline campaign (mg $N_2O$ /m<sup>3</sup>)

OH<sub>BC</sub> - Operating hours of the baseline campaign (h)

VSG<sub>BC</sub> - Mean gas volume flow rate at the stack in the baseline measurement period (m<sup>3</sup>/h)

NAP<sub>BC</sub> - Nitric acid production during the baseline campaign (t $HNO_3$ )

UNC - Overall uncertainty of the monitoring system (%), calculated as the combined uncertainty of the applied monitoring equipment

In June 2008, the plant will be stopped for second maintenance period, during which modification of oxidation reactors will take place and secondary catalysts will be installed. After the installation of secondary catalysts – the monitoring of project emissions will take place.

As the methodology requires monitoring of baseline emissions for entire lifespan of platinum gauzes i.e. for 11 months, the exact baseline can be determined only after the entire baseline monitoring period. In order to project  $N_2O$  emission reductions a stationary analyser SICK-Mayhak UNOR 6N (infrared) was used to measure  $N_2O$  concentration in the tail gas flow in April 2007. Real data will be available after the end of the baseline campaign.

If the length of each individual project campaign  $CL_n$  is longer than or equal to the average historic campaign length  $CL_{normal}$ , then all  $N_2O$  values measured during the baseline campaign can be used for the calculation of EF (subject to the elimination of data from the Ammonia/Air analysis).

If  $CL_n < CL_{normal}$ , EF<sub>BL</sub> will be recalculated by eliminating those  $N_2O$  values that were obtained during the production of tonnes of nitric acid beyond the  $CL_n$  (i.e. the last tonnes produced) from the calculation of EF<sub>n</sub>.



The global warming potential value of N<sub>2</sub>O (1 t N<sub>2</sub>O = 310 t CO<sub>2</sub>e) will be used to translate N<sub>2</sub>O emissions to CO<sub>2</sub> equivalents.

**B.2. Description of how the anthropogenic emissions of greenhouse gases by sources are reduced below those that would have occurred in the absence of the JI project:**

The Nitrous Oxide Emission Reduction Project at GP Nitric acid plant in Achema fertiliser plant is completely additional as at the present there exist no economic, technical, institutional or other incentives in Lithuania to reduce N<sub>2</sub>O emissions below the current levels. The Tool for the demonstration and assessment of additionality (version 3) is used to describe how the anthropogenic emissions of greenhouse gases are reduced below those that would have occurred in the absence of the JI project.

**Step 1. Identification of alternatives to the project activity consistent with current laws and regulations**

***Sub-step 1a. Define alternatives to the project activity:***

The AM0034 states: "The baseline scenario shall be identified using procedure for Identification of the baseline scenario described in the approved methodology AM0028 "Catalytic N<sub>2</sub>O destruction in the tail gas of Nitric Acid Plants". Step 1a of AM0028 lists the following alternatives:

- A) The continuation of the current situation, where there will be no installation of technology for the destruction or abatement of N<sub>2</sub>O.
- B) Switch to alternative production method not involving ammonia oxidation process
- C) Alternative use of N<sub>2</sub>O such as:
  - a. Recycling of N<sub>2</sub>O as a feedstock for the plant;
  - b. The use of N<sub>2</sub>O for external purposes.
- D) Installation of a Non-Selective Catalytic Reduction (NSCR) DeNO<sub>x</sub> unit.
- E) The installation of an N<sub>2</sub>O destruction or abatement technology:
  - a. Tertiary measure for N<sub>2</sub>O destruction;
  - b. Primary or secondary measures for N<sub>2</sub>O destruction or abatement.
- F) Implementation of the JI project under the introduced obligatory N<sub>2</sub>O limit values.

***Sub-step 1b. Consistency with mandatory laws and regulations:***

There are two issues that have a potential to affect the project. These are: IPPC regulation and possible inclusion of N<sub>2</sub>O into the EU Emission Trading Scheme.

In August 2007, the reference document on Best Available Techniques for the "Manufacture of Large Volume Inorganic Chemicals – Ammonia, Acids and Fertilisers" (LVIC BREF) was approved. LVIC BREF describes Best Available Techniques (BAT) and suggests the upper N<sub>2</sub>O limit value of 1.85kg N<sub>2</sub>O/t HNO<sub>3</sub> (100%) for existing nitric acid plants. While authorities of the EU member states including Lithuania have to take BREF documents into consideration when issuing IPPC permits, there are also several legal aspects to be taken into account.

Para 4 of the Article 9 of the Directive 96/61/EC states that: "Without prejudice to Article 10, the emission limit values and the equivalent parameters and technical measures referred to in paragraph 3



shall be based on the best available techniques, without prescribing the use of any technique or specific technology, but taking into account the technical characteristics of the installation concerned, its geographical location and the local environmental conditions".

Chapter 6 (The "Sevilla Process") of the Communication from the Commission to the Council, the European Parliament, the European Economic and Social Committee and the Committee of the Regions COM/2003/0354 "On the Road to Sustainable Production - Progress in implementing Council Directive 96/61/EC concerning integrated pollution prevention and control", states the following: "However, BREF documents do not set any legally binding standards. They simply provide reference information. Since authorities are also expected to take account of the technical characteristics of the installation, its geographical location and the local environmental conditions, BREF documents cannot be the only basis for emission limit values and other permit conditions."

The term "technical characteristics" stated in the Directive, which have to be taken into account, in case of N<sub>2</sub>O abatement technology for nitric acid plants would mean the complexity of N<sub>2</sub>O abatement technology itself and issues related to its implementation. It should be noted that no of-the-shelf product is available on the market for secondary catalysts and each abatement case requires a specific technical approach and design. Design, order, construction and testing of abatement technology is a costly, time consuming process that involves a number of technical and economic risks.

The JI mechanism gives an economic incentive for a company to abate N<sub>2</sub>O in the fastest and most efficient way achieving maximum emission reductions. It also allows to accept considerably higher level of technical risks and costs that otherwise would be unacceptable. JI mechanism also allows to reduce capital costs of abatement technology as a supplier of the technology can be involved as a project participant.

In contrast, IPPC permitting scheme does not give any economic incentive for emission abatement. Companies have to comply with standards at reasonable costs and would not go further than the requirements imposed. Hence, it should be taken into consideration that introduction of IPPC limit values gives different timing, efficiency and quantity of emission reductions compared to the JI mechanism. Nevertheless, the baseline under the JI mechanism is affected by the IPPC regulation and has to be evaluated.

The IPPC permit of AB Achema was issued on 28 December 2004 by the Kaunas Regional Department for Environmental protection. On 30 April 2008, an updated IPPC permit was issued that imposed N<sub>2</sub>O limit values. The summary is presented in Table 4.

**Table 4 N<sub>2</sub>O limit values (t N<sub>2</sub>O) for the GP plant in the IPPC permit**

2008	2009	2010	2011	2012	2013
3174.5	3174.5	3174.5	2926	2040.5	1256.5

IPPC limit values were reflected in the baseline and emission reduction projections. IPPC limit values were considered as a new baseline level in cases where these limits were lower than the estimated baseline, namely in year 2012. Figures presented in Chapter A.4.3.1 reflect this impact of the IPPC regulation on the estimated emission reductions.

As pointed earlier, another issue that can potentially affect the baseline is the inclusion of N<sub>2</sub>O into EU ETS. Para 1 of the Article 24 of the Directive 2003/87/EC states that: "From 2008, Member States may apply emission allowance trading in accordance with this Directive to activities, installations and greenhouse gases which are not listed in Annex I, provided that inclusion of such activities, installations and greenhouse gases is approved by the Commission (...)" Lithuanian National Allocation Plan for



2008-2012 under EU ETS does not contain any provisions for inclusion of N<sub>2</sub>O into EU ETS in Lithuania for the period 2008-2012.

## **Step 2. Investment analysis**

### ***Sub-step 2a. Determine appropriate analysis method***

*Simple cost analysis (option I)* is applied for the project as the activity produces no economic benefits other than JI related income.

The costs of secondary catalysts, reactor reconstruction works, design and installation are in range of several million EUR. In addition to that there are significant costs related to the JI project development. There are no subsidies or other support available for such technologies. The only revenues from the project are ERU sales, which are to be generated during the JI activity. As no other revenues are available for the project, it is economically feasible only under the JI mechanism.

## **Step 3. Barrier analysis**

### ***Sub-step 3a.***

Alternative B is not feasible as currently there are no commercially available technologies for nitric acid production other than ammonia oxidation. Earlier used Glauber method (saltpetre reacting with sulphuric acid) and Birkland & Edye method (electrical discharge on air) proved to be costly and inefficient. Thus, this alternative is not feasible.

Alternative C is not feasible as it is not possible produce nitric acid from N<sub>2</sub>O, therefore there is no reason to keep it as a feedstock. Also, there no case studies of N<sub>2</sub>O recovery as a feedstock. N<sub>2</sub>O use for external purposes is not profitable economically as N<sub>2</sub>O concentrations are very low compared to the amount of tail gas and thus recovery of it requires many efforts.

Alternative D is not feasible as AB Achema is already operating a selective catalytic reduction De NO<sub>x</sub> unit and complies with the existing NO<sub>x</sub> regulation. There is no economic reason to use more costly and less effective Non-selective catalytic reduction unit.

Alternative E is not feasible as N<sub>2</sub>O emission reduction in the HNO<sub>3</sub> production process is a costly procedure and does not give any revenues, except from ERU sales. This implies that the project can be implemented only under the JI mechanism. Moreover, if abatement technology is not correctly designed and installed it can influence production level and product quality.

### ***Sub-step 3b.***

Alternative A is feasible as any of the existing N<sub>2</sub>O abatement technologies imply additional costs and no revenues outside the JI mechanism. There are no subsidies or other support measures available for N<sub>2</sub>O abatement technologies in Lithuania. The existing regulation does not demand N<sub>2</sub>O emission reductions either, hence the producer has no incentive for N<sub>2</sub>O emission reductions.

Alternative F is feasible if the N<sub>2</sub>O limit values are set in the IPPC permit issued to AB Achema. The details and timing of such alternative are not clear yet. If the N<sub>2</sub>O limit values are introduced by the regulatory requirements, then the baseline will be recalculated accordingly, setting the obligatory limit value as a new baseline.



**Step 4. Common practice analysis****Sub-step 4a. Analyze other activities similar to the proposed project activity:**

Achema fertiliser plant is the only producer of Nitric acid in Lithuania, so no other N<sub>2</sub>O abatement projects were carried out or are to be carried out in Lithuania. There are no common practices in Europe to implement N<sub>2</sub>O reduction projects in business-as-usual case. Projects are developed under the JI mechanism, and it can be assumed that these projects would not be implemented without JI.

**Sub-step 4b. Discuss any similar options that are occurring:**

Not applicable.

**B.3. Description of how the definition of the project boundary is applied to the project:**

“The project boundary shall encompass all anthropogenic emissions by sources and/or removals by sinks of greenhouse gases under the control of the project participants that are significant and reasonably attributable to the JI project.” (Guidelines for users of the Joint Implementation project design document for, Version 01)

Project boundary covers entire GP plant (the diagram of the plant is presented in Figure 5 in chapter A.4.2). The only significant and reasonably attributable to the JI project GHG source within the project boundary is N<sub>2</sub>O emissions.

	Source	Gas	Included?	Justification / Explanation
<b>Baseline</b>	Nitric Acid Plant (Burner Inlet to Stack)	CO <sub>2</sub>	Excluded	The project does not lead to any change in CO <sub>2</sub> or CH <sub>4</sub> emissions, and, therefore, these are not included.
		CH <sub>4</sub>	Excluded	
		N <sub>2</sub> O	Included	
<b>Project Activity</b>	Nitric Acid Plant (Burner Inlet to Stack)	CO <sub>2</sub>	Excluded	The project does not lead to any change in CO <sub>2</sub> or CH <sub>4</sub> emissions
		CH <sub>4</sub>	Excluded	
		N <sub>2</sub> O	Included	
	Leakage emissions from production, transport, operation and decommissioning of the catalyst.	CO <sub>2</sub>	Excluded	No leakage emissions are expected.
		CH <sub>4</sub>	Excluded	
		N <sub>2</sub> O	Excluded	

**B.4. Further baseline information, including the date of baseline setting and the name(s) of the person(s)/entity(ies) setting the baseline:**

The baseline study was prepared by consulting a company UAB Ekostrategija (acquired by COWI Baltic in 11 2007) and completed on 01 06 2007.

Company name	<i>COWI Baltic</i>
Street	Lukiskiu
Building No	3



State/Region/City	Vilnius
Post code	LT-01108
Country	Lithuania
Telephone number	+370 5 2107610
Fax number	+370 5 2124777
E-mail	info@cowi.lt
Website	www.cowi.lt
Representative	Vaidotas Kuodys
Position	Project manager
Salutation	
Surname	Kuodys
Second name	-
First name	Vaidotas
Subdivision	-
Telephone number (direct)	+370 5 2191307
Fax number (direct)	+370 5 2124777
E-mail (personal)	kuodys.v@gmail.com

**SECTION C. Duration of the project / crediting period****C.1. Starting date of the project:**

Installation of the secondary catalysts is envisioned for July 2008.

**C.2. Expected operational lifetime of the project:**

20 years

**C.3. Length of the crediting period:**

Four years and four and a half months: 16.08.2008 – 31.12.2012.

**SECTION D. Monitoring plan****D.1. Description of monitoring plan chosen:**

Approved monitoring methodology AM0034 “Catalytic reduction of N<sub>2</sub>O inside the ammonia burner of nitric acid plants” is used for the project.

**D.1.1. Option 1 – Monitoring of the emissions in the project scenario and the baseline scenario:****D.1.1.1. Data to be collected in order to monitor emissions from the project, and how these data will be archived:**

ID number <i>(Please use numbers to ease cross-referencing to D.2.)</i>	Data variable	Source of data	Data unit	Measured (m), calculated (c), estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment
P.1	NCSG  N <sub>2</sub> O concentration in tail gas	N <sub>2</sub> O analyser  AO-2040-URAS- 14	mg N <sub>2</sub> O /m <sup>3</sup> (converted from ppm )	m	Every 2 seconds	100%	Electronic	The data output from analyser will be processed using Anayse IT Explorer
P.2	VSG  Volume flow rate of the stack gas	Gas volume flow meter DELTAFLOW	nm <sup>3</sup> /h	m	Every 2 seconds	100%	Electronic	The data output from flow meter will be processed using Anayse IT Explorer
P.3	PE <sub>n</sub>  N <sub>2</sub> O emissions of nth project campaign	Calculation from measured data	t N <sub>2</sub> O	c	Once after each campaign	100%	Electronic and paper	
P.4	OH	Production log	Hours	m	Daily, compiled for entire	100%	Electronic and paper	

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	<i>Operating hours</i>				<i>campaign</i>			
P.5	<i>NAP Nitric Acid production (100% concentrate)</i>	<i>Production log</i>	<i>tHNO<sub>3</sub></i>	<i>m</i>	<i>Daily, compiled for entire campaign</i>	<i>100%</i>	<i>Electronic and paper</i>	<i>Total production over project campaign.</i>
P.6	<i>TSG Temperature of Stack gas</i>	<i>Probe (part of gas volume flow meter) DELTAFLOW</i>	<i>C<sup>0</sup></i>	<i>m</i>	<i>Every 2 seconds</i>	<i>100%</i>	<i>Electronic and paper</i>	
P.7	<i>PSG Pressure of stack gas</i>	<i>Probe (part of gas volume flow meter) DELTAFLOW</i>	<i>Pa</i>	<i>m</i>	<i>Every 2 seconds</i>	<i>100%</i>	<i>Electronic and paper</i>	
P.8	<i>EF<sub>n</sub> Emissions factor calculated for nth campaign</i>	<i>Calculated from measured data</i>	<i>t N<sub>2</sub>O / tHNO<sub>3</sub></i>	<i>c</i>	<i>After end of each campaign</i>			
P.9	<i>EF<sub>m,a</sub> Moving average emissions factor</i>	<i>Calculated from campaign emissions factors</i>	<i>t N<sub>2</sub>O / tH NO<sub>3</sub></i>	<i>c</i>	<i>After end of each campaign</i>			
P.10	<i>CLn Campaign length</i>	<i>Calculated from nitric acid production data</i>	<i>tHNO<sub>3</sub></i>	<i>c</i>	<i>After end of each campaign</i>	<i>100%</i>	<i>Electronic and paper</i>	

**D.1.1.2. Description of formulae used to estimate project emissions (for each gas, source etc.; emissions in units of CO<sub>2</sub> equivalent):**

Monitoring system will continue function after the installation of the secondary catalysts. Readings of N<sub>2</sub>O concentration and gas volume flow will be automatically corrected by eliminating error and extreme values. The same statistical data processing method will be applied as to the baseline measurement results (B.1).

Project emissions shall be using the following formula:

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$$PE_n = VSG * NCSG * 10^{-9} * OH \text{ (tN}_2\text{O)} \quad (3)$$

Where:

PE<sub>n</sub> - Total N<sub>2</sub>O emissions of the nth project campaign (tN<sub>2</sub>O)  
VSG - Mean stack gas volume flow rate for the project campaign (m<sup>3</sup>/h)  
NCSG - Mean concentration of N<sub>2</sub>O in the stack gas for the project campaign (mgN<sub>2</sub>O/m<sup>3</sup>)  
OH - Number of hours of operation in the specific monitoring period (h)

In order to take into account possible long-term emissions trends over the duration of the project activity and to take a conservative approach a moving average emission factor shall be estimated as follows:

Step1: campaign specific emissions factor for each campaign during the project's crediting period will be estimated by dividing the total mass of N<sub>2</sub>O emissions during that campaign by the total production of 100% concentrated nitric acid during that same campaign:

$$EF_n = PE_n / NAP_n \text{ (tN}_2\text{O/tHNO}_3\text{)} \quad (4)$$

Where:

NAP<sub>n</sub> - Nitric acid production during the n<sup>th</sup> campaign (tHNO<sub>3</sub>)

Step 2: a moving average emissions factor will be calculated at the end of a campaign n as follows:

$$EF_{ma,n} = (EF_1 + EF_2 + \dots + EF_n) / n \text{ (tN}_2\text{O/tHNO}_3\text{)} \quad (5)$$

This process will be repeated for each campaign such that a moving average, EF<sub>ma,n</sub>, is established over time, becoming more representative and precise with each additional campaign. To calculate the total emission reductions achieved in a campaign in formula (7) below, the higher of the two values EF<sub>ma,n</sub> and EF<sub>n</sub> shall be applied as the emission factor relevant for the particular campaign to be used to calculate emissions reductions (EF<sub>p</sub>):

$$\text{If } EF_{ma,n} > EF_n \text{ then } EF_p = EF_{ma,n} \quad (6)$$

$$\text{If } EF_{ma,n} < EF_n \text{ then } EF_p = EF_n$$

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Where:

$EF_n$  - Emission factor calculated for a specific project campaign ( $tN_2O/tHNO_3$ )

$EF_{ma,n}$  - Moving average (ma) emission factor of after  $n^{th}$  campaigns, including the current campaign ( $tN_2O/tHNO_3$ )

$n$  - Number of campaigns to date

$EF_p$  - Emissions factor that will be applied to calculate the emissions reductions from the specific campaign ( $N_2O/tHNO_3$ )

<b>D.1.1.3. Relevant data necessary for determining the <u>baseline</u> of anthropogenic emissions of greenhouse gases by sources within the project boundary, and how such data will be collected and archived:</b>								
ID number (Please use numbers to ease cross-referencing to D.2.)	Data variable	Source of data	Data unit	Measured (m), calculated (c), estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment
B.1	$NCSG_{BC}$  $N_2O$ concentration in the stack gas	$N_2O$ analyser  AO-2000-URAS-14	$mg N_2O / m^3$ (converted from ppm )	m	Every 2 seconds	100%	Electronic	The data output from analyser will be processed using Anayse IT Explorer
B.2	$VSG_{BC}$  Volume flow rate of the stack gas	Gas volume flow meter DELTAFLOW	$nm^3/h$	m	Every 2 seconds	100%	Electronic	The data output from flow meter will be processed using Anayse IT Explorer
B.3	$BE_{BC}$  Total $N_2O$ for baseline campaign	Calculation from measured data	$t N_2O$	c	Once after each campaign	100%	Electronic and paper	
B.4	$OH_{BC}$  Operating hours	Production log	Hours	m	Daily, compiled for entire campaign	100%	Electronic and paper	

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B.5	$NAP_{BC}$ Nitric Acid production (100% concentrate)	Production log	$t HNO_3$	m	Daily, compiled for entire campaign	100%	Electronic and paper	Total production over project campaign.
B.6	TSG Temperature of Stack gas	Probe (part of gas volume flow meter) DELTAFLOW	$C^0$	m	Every 2 seconds	100%	Electronic and paper	
B.7	PSG Pressure of stack gas	Probe (part of gas volume flow meter) DELTAFLOW	Pa	m	Every 2 seconds	100%	Electronic and paper	
B.8	$EF_{BL}$ Emissions factor calculated for nth campaign	Calculated from measured data	$t N_2O / t HNO_3$	c	After end of each campaign			
B.9	UNC Overall measurement uncertainty of the monitoring system	Calculation of the combined uncertainty of the applied monitoring equipment	%	c	Once after monitoring system is commissioned		Electronic and paper	
B.10	AFR Ammonia gas flow rate to the AOR	Monitored	$kgNH_3/h$	m	Every hour	100%	Electronic and paper	To be obtained from the operating condition campaign
B.11	AIFR Ammonia gas flow rate to the AOR	Monitored	$m^3/h$	m/c	Every hour	100%	Electronic and paper	To be obtained from the operating condition campaign



B.12	<i>OT<sub>h</sub></i> <i>Oxidation temperature for each hour</i>	<i>Monitored</i>	°C	<i>m</i>	<i>Every hour</i>	<i>100%</i>	<i>Electronic and paper</i>	<i>To be obtained from the operating condition campaign</i>
B.13	<i>OP<sub>h</sub></i> <i>Oxidation Pressure for each hour</i>		Pa	<i>m</i>	<i>Every hour</i>	<i>100%</i>	<i>Electronic and paper</i>	<i>To be obtained from the operating condition campaign</i>

**D.1.1.4. Description of formulae used to estimate baseline emissions (for each gas, source etc.; emissions in units of CO<sub>2</sub> equivalent):**

Baseline emissions will be estimated by using the following formula:

$$BE_{BC} = VSG_{BC} * NCSG_{BC} * 10^{-9} * OH_{BC}$$

Where:

BE<sub>BC</sub> - Total N<sub>2</sub>O emissions during the baseline campaign (tN<sub>2</sub>O)

NCSG<sub>BC</sub> - Mean concentration of N<sub>2</sub>O in the stack gas during the baseline campaign (mgN<sub>2</sub>O/m<sup>3</sup>)

OH<sub>BC</sub> - Operating hours of the baseline campaign (h)

VSG<sub>BC</sub> - Mean gas volume flow rate at the stack in the baseline measurement period (m<sup>3</sup>/h)

**D. 1.2. Option 2 – Direct monitoring of emission reductions from the project (values should be consistent with those in section E.):**

**D.1.2.1. Data to be collected in order to monitor emission reductions from the project, and how these data will be archived:**

ID number <i>(Please use numbers to ease cross-referencing to D.2.)</i>	Data variable	Source of data	Data unit	Measured (m), calculated (c), estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment

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**D.1.2.2. Description of formulae used to calculate emission reductions from the project (for each gas, source etc.; emissions/emission reductions in units of CO<sub>2</sub> equivalent):**

**D.1.3. Treatment of leakage in the monitoring plan:**

**D.1.3.1. If applicable, please describe the data and information that will be collected in order to monitor leakage effects of the project:**

ID number (Please use numbers to ease cross-referencing to D.2.)	Data variable	Source of data	Data unit	Measured (m), calculated (c), estimated (e)	Recording frequency	Proportion of data to be monitored	How will the data be archived? (electronic/ paper)	Comment

**D.1.3.2. Description of formulae used to estimate leakage (for each gas, source etc.; emissions in units of CO<sub>2</sub> equivalent):**

No leakage calculation is required.

**D.1.4. Description of formulae used to estimate emission reductions for the project (for each gas, source etc.; emissions/emission reductions in units of CO<sub>2</sub> equivalent):**

Emission reductions will be calculated by using the following formula:

$$ER = (EF_{BL} - EF_P) * NAP * GWP_{N_2O} \quad (tCO_2e)$$

ER - Emission reductions of the project for the specific campaign (tCO<sub>2</sub>e)

NAP - Nitric acid production for the project campaign (tHNO<sub>3</sub>)

EF<sub>BL</sub> - Baseline emissions factor (tN<sub>2</sub>O/tHNO<sub>3</sub>)

EF<sub>P</sub> - Emissions factor used to calculate the emissions from this particular campaign

GWP<sub>N<sub>2</sub>O</sub> - Global warming potential of the N<sub>2</sub>O (310)



**D.1.5. Where applicable, in accordance with procedures as required by the host Party, information on the collection and archiving of information on the environmental impacts of the project:**

N/A

**D.2. Quality control (QC) and quality assurance (QA) procedures undertaken for data monitored:**

Data (Indicate table and ID number)	Uncertainty level of data (high/medium/low)	Explain QA/QC procedures planned for these data, or why such procedures are not necessary.
P1, B1	Low	QAL1, QAL2 and QAL3 procedures are performed according to European Norm 14181
P2, B2	Low	QAL1, QAL2 and QAL3 procedures are performed according to European Norm 14181
P6, B6	Low	QAL1, QAL2 and QAL3 procedures are performed according to European Norm 14181
P7, B7	Low	QAL1, QAL2 and QAL3 procedures are performed according to European Norm 14181
B9	Low	Assured by the producers and designer of the monitoring scheme
B10	Low	Ammonia input is measured with Ammonia flow meter which is regularly calibrated and tested
B11	Low	Oxidation temperature is measured with the device which is regularly calibrated and tested
B12	Low	Oxidation pressure is measured with Ammonia flow meter which is regularly calibrated and tested

**D.3. Please describe the operational and management structure that the project operator will apply in implementing the monitoring plan:**

“Sistematika” a division of AB Achema is in charge of operation and maintenance of the N<sub>2</sub>O monitoring system. The Nitric acid production department is responsible for the N<sub>2</sub>O monitoring and for reporting faults in the operation of the monitoring system to “Sistematika”. Monitoring will be performed by the DCS operators and the technical support will be provided by the directly responsible automation engineer.

**D.4. Name of person(s)/entity(ies) establishing the monitoring plan:**

Company name	COWI Baltic
Street	Lukiskiu
Building No	3
State/Region/City	Vilnius
Post code	LT-01108



Country	Lithuania
Telephone number	+370 5 2107610
Fax number	+370 5 2124777
E-mail	info@cowi.lt
Website	www.cowi.lt
Representative	Vaidotas Kuodys
Position	Project manager
Salutation	
Surname	Kuodys
Second name	-
First name	Vaidotas
Subdivision	-
Telephone number (direct)	+370 5 2191307
Fax number (direct)	+370 5 2124777
E-mail (personal)	kuodys.v@gmail.com

**SECTION E. Estimation of greenhouse gas emission reductions****E.1. Estimated project emissions:**

Project emissions are directly related to the efficiency of the secondary catalyst installed. The secondary catalyst is expected to perform with up to 80% efficiency. This would imply that in the optimistic scenario the remaining 20% of N<sub>2</sub>O will be released to the atmosphere. According to the preliminary estimations, project emissions would constitute 466.59 t N<sub>2</sub>O / year or 144,642 t CO<sub>2</sub>e / year. It should be noted that this figure is illustrative and depend on Nitric acid production volumes and other factors that can influence it.

**E.2. Estimated leakage:**

E.2 = 0

**E.3. The sum of E.1. and E.2.:**

E.1 + E.2 = 144,642 t CO<sub>2</sub>e + 0 = 144,642 t CO<sub>2</sub>e

**E.4. Estimated baseline emissions:**

Estimated annual baseline emissions 723,211 t CO<sub>2</sub>e / year (2332.94 tN<sub>2</sub>O / year).

**E.5. Difference between E.4. and E.3. representing the emission reductions of the project:**

E.4 – E.3 = 723,211- 144,642 = 578,569 CO<sub>2</sub>e / year

**E.6. Table providing values obtained when applying formulae above:**

Year	Estimated project emissions (tonnes of CO <sub>2</sub> equivalent)	Estimated leakage(tonnes of CO <sub>2</sub> equivalent)	Estimated baseline emissions (tonnes of CO <sub>2</sub> equivalent)	Estimated emission reductions (tonnes of CO <sub>2</sub> equivalent)
2008	60,491	0	302,455	241,964
2009	144,642	0	723,211	578,569
2010	144,642	0	723,211	578,569
2011	144,642	0	723,211	578,569
2012	144,642	0	632,555	487,913
Total	639,059	0	3,104,644	2,465,585
Annual average	146,071	0	709,633	563,562

2008 emissions are different due to the start of the project operation in second half of the 2008, and 2012 emission reductions are different due to the impact of the IPPC regulation described in B2.

**SECTION F. Environmental impacts****F.1. Documentation on the analysis of the environmental impacts of the project, including transboundary impacts, in accordance with procedures as determined by the host Party:**



No negative environmental impacts are envisioned. Lithuanian Law on Environmental Impact Assessment (EIA) requires EIA to be carried out for the planned economic activity. Planned economic activity is described in the law as "...modification of the production process and modernisation or replacement of the technology, modification of production method, alteration of production quantity or production type..." Representatives of AB Achema have had discussions with officials of regional environmental protection department. The conclusion was made that installation of the secondary catalyst is not to be considered as economic activity as it does not alter production level nor makes modification to production lines. Therefore no EIA or selection procedure for EIA is required.

**F.2. If environmental impacts are considered significant by the project participants or the host Party, please provide conclusions and all references to supporting documentation of an environmental impact assessment undertaken in accordance with the procedures as required by the host Party:**

N/a

#### **SECTION G. Stakeholders' comments**

##### **G.1. Information on stakeholders' comments on the project, as appropriate:**

AB Achema has initiated a comprehensive stakeholder process on the issue of IPPC regulation and JI baseline related to N<sub>2</sub>O reduction projects in AB Achema. A number of meetings were held during the period of November 2007 to February 2008. The representatives of the following organizations participated in the meetings: regulating institutions, AB Achema, association of industries, consultants and other stakeholders. The following official institutions were involved: Ministry of Environment, Environmental Protection Agency and Regional Department for Environmental Protection.

The aim of the stakeholder process was to clarify the IPPC requirements for N<sub>2</sub>O limit values, its impact on the baseline of N<sub>2</sub>O reduction projects and the position of the authorities towards the issue. At the present the IPPC permit issued to AB Achema does not contain any restrictions related to N<sub>2</sub>O. It is also confirmed in the letter from the Kaunas Regional department for Environmental Protection, dated January 25, 2008. However, Lithuanian authorities are aware of the IPPC requirements and are considering options of regulating N<sub>2</sub>O in the updated Achema's IPPC permit.

Annex 1**CONTACT INFORMATION ON PROJECT PARTICIPANTS**

Organisation:	AB Achema
Street/P.O.Box:	
Building:	
City:	
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Annex 2

**BASELINE INFORMATION**

Baseline monitoring data is expected to be available in 2008.



### Annex 3

#### **MONITORING PLAN**

The N<sub>2</sub>O monitoring system in AB Achema GP plant is implemented according to European Norm 14181 and AM0034 methodology. All three Quality Assurance Levels (QAL1, QAL2 and QAL3) and Annual Surveillance Test (AST) shall be applied to ensure that the monitoring system functions in line with the standards. QAL1 is ensured by the suppliers of the monitoring equipment, QAL2 is performed by an accredited monitoring institute and QAL3 to be performed by the responsible personnel of AB Achema and during the automatic calibration procedures of the monitoring equipment. AST shall be performed annually by a selected certification body. Short summary:

- ✓ QAL1 procedure requires compliance of the equipment with EN ISO 14956. AO-2000-URAS-14 and DELTAFLOW are ISO 14956 certified by the manufacturers.
- ✓ QAL2 procedure requires determination of the calibration function and a test of the measured values of the AMS compared with the uncertainty given by legislation. During the maintenance period of the GP plant (September 2007) the openings required for QAL2 tests will be made in the duct. QAL2 procedure will be performed by TUV at the end of the next campaign.
- ✓ QAL3 is a procedure to check drift and precision in order to demonstrate that the AMS is in control during its operation so that it continues to function within the required specifications for uncertainty. QAL3 procedures will be performed automatically as the system will calibrate itself once a week. In addition, Achema experts will perform maintenance of the equipment – will fix faults, change filters, remove condensate from the system etc.
- ✓ AST is a procedure to evaluate whether the measured values obtained from the AMS still meet the required uncertainty criteria – as demonstrated in the previous QAL2 test. AST will be performed annually by selected certifier.

N<sub>2</sub>O emission monitoring is performed automatically by the installed equipment. A flow meter measures volume flow (m<sup>3</sup>/h), temperature and pressure in the tail gas and sends signals to the server. The server stores data and forwards signal to the Distributed Control System (DCS). The N<sub>2</sub>O analyzer continuously measures concentration of N<sub>2</sub>O in the tail gas and also sends signal to the data server which forwards it to DCS.

The monitoring system shall be operated and maintained by “Sistematika” a division of AB Achema. Data collection and fault reporting to “Sistematika” is a responsibility of the Nitric acid production department. Monitoring will be performed by the DCS operators while the technical support will be provided by automation engineers.

After the baseline monitoring period is over, records of the monitored data (N<sub>2</sub>O) concentration and tail gas flow volume) shall be statistically examined according to AM0034 methodology:

- a) Sample mean ( $\bar{x}$ ) calculated
- b) Sample standard deviation (s) calculated
- c) 95% confidence interval (equal to 1.96 times the standard deviation) calculated
- d) All data that lie outside the 95% confidence interval will be eliminated
- e) New sample mean from the remaining values of volume of stack gas (VSG) and N<sub>2</sub>O concentration of stack gas (NCSG) will be calculated





In order to avoid the possibility that the operating conditions of the nitric acid production plant are modified in such a way that increases N<sub>2</sub>O generation during the baseline campaign, the normal ranges for operating conditions shall be determined for the following parameters:

- a) oxidation temperature
- b) oxidation pressure
- c) ammonia gas flow rate
- d) air input flow rate

The permitted range of the parameters shall be established in combination of all three data sources specified in the AM0034 methodology:

- a) Historical data of the operating range from the previous campaigns;
- b) The range stipulated in the operating manual for the existing equipment;
- c) Appropriate technical literature

The historical data shall be processed in line with the requirements stipulated in AM0034.